

# General Modelling and Scaling Laws

- Dimensionless numbers
- Similarity requirements
- Derivation of dimensionless numbers used in model testing
- Froude scaling
- Hydroelasticity
- Cavitation number

# Dimensionless numbers

- *”Without dimensionless numbers, experimental progress in fluid mechanics would have been almost nil; It would have been swamped by masses of accumulated data”* (R. Olson)
- Example:  
Due to the beauty of dimensionless numbers,  $C_f$  of a flat, smooth plate is a function of  $Re$  only  
(not function of temperature, pressure or type of fluid<sup>1</sup>)

<sup>1</sup>As long as the fluid is Newtonian, which means that it has a linear stress/strain rate, with zero stress for zero strain

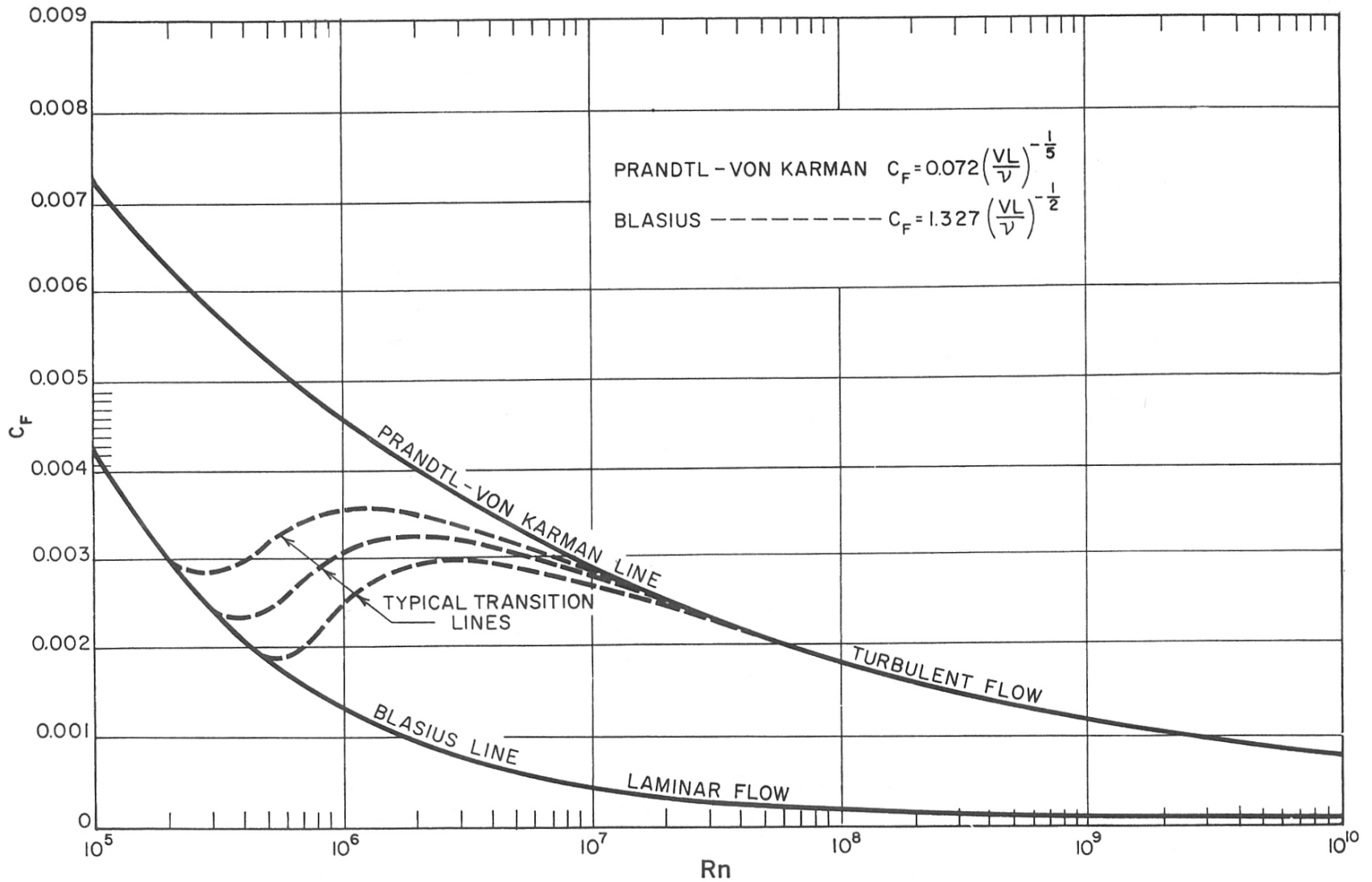


Fig. 2 Skin friction lines, turbulent and laminar flow

# Types of similarity

- Geometrical similarity
- Kinematic similarity
- Dynamic similarity

What are the similarity requirements for a model test?

# Geometrical Similarity

- The model and full scale structures must have the same shape

⇒ All linear dimensions must have the same scale ratio:

$$\lambda = L_F / L_M$$

- This applies also to:
  - The environment surrounding the model and ship
  - Elastic deformations of the model and ship

# Kinematic Similarity

- Similarity of velocities:

⇒ The flow and model(s) will have geometrically similar motions in model and full scale

## Examples:

- Velocities in x and y direction must have the same ratio, so that a circular motion in full scale must be a circular motion also in model scale
- The ratio between propeller tip speed and advance speed must be the same in model and full scale:

$$\frac{V_F}{n_F (2\pi R_F)} = \frac{V_M}{n_M (2\pi R_M)} \quad \text{or} \quad \frac{V_F}{n_F D_F} = \frac{V_M}{n_M D_M} \Rightarrow J_F = J_M$$

# Dynamic Similarity

- Geometric similarity  
and
  - Similarity of forces
    - $\Rightarrow$  *Ratios between different forces in full scale must be the same in model scale*
- $\Rightarrow$  If you have geometric and dynamic similarity, you'll also have kinematic similarity
- The following force contributions are of importance:
    - Inertia Forces,  $F_i$
    - Viscous forces,  $F_v$
    - Gravitational forces,  $F_g$
    - Pressure forces,  $F_p$
    - Elastic forces in the fluid (compressibility),  $F_e$ .
    - Surface forces,  $F_s$ .

# Inertia Forces (mass forces)

$$F_i \propto \rho \frac{dU}{dt} L^3 = \rho \frac{dU}{dx} \frac{dx}{dt} L^3 \propto \rho U^2 L^2$$

- $\rho$  is fluid density
- $U$  is a characteristic velocity
- $t$  is time
- $L$  is a characteristic length (linear dimension)



# Gravitational Forces

$$F_g \propto \rho g L^3$$

⇒ Just mass times acceleration

- $g$  is acceleration of gravity

# Viscous Forces

$$F_v \propto \mu \frac{dU}{dx} L^2 \propto \mu UL$$

- $\mu$  is dynamic viscosity [kg/m·s]  
 - a function of temperature and type of fluid

# Pressure Forces

$$F_p \propto pL^2$$

$\Rightarrow$  Force equals pressure times area

- $p$  is pressure

# Elastic Fluid Forces

$$F_e \propto \varepsilon_v E_v L^2$$

- $\varepsilon_v$  is compression ratio
- $E_v$  is the volume elasticity (or compressibility)
- $\varepsilon_v \cdot E_v$  = elasticity modulus  $K$  [kg/m·s<sup>2</sup>]

# Surface Forces

$$F_s \propto \sigma L$$

- $\sigma$  is the surface tension [kg/s<sup>2</sup>]

# Froude number $F_n$

- The ratio between inertia and gravity:

$$\frac{\text{Inertia force}}{\text{Gravity force}} = \frac{F_i}{F_g} \propto \frac{\rho U^2 L^2}{\rho g L^3} = \frac{U^2}{gL}$$

- Dynamic similarity requirement between model and full scale:

$$\frac{U_M^2}{gL_M} = \frac{U_F^2}{gL_F}$$

$$\frac{U_M}{\sqrt{gL_M}} = \frac{U_F}{\sqrt{gL_F}} = F_n$$

- Equality in  $F_n$  in model and full scale will ensure that gravity forces are correctly scaled
- Surface waves are gravity-driven  $\Rightarrow$  equality in  $F_n$  will ensure that wave resistance and other wave forces are correctly scaled

# Reynolds number $Re$

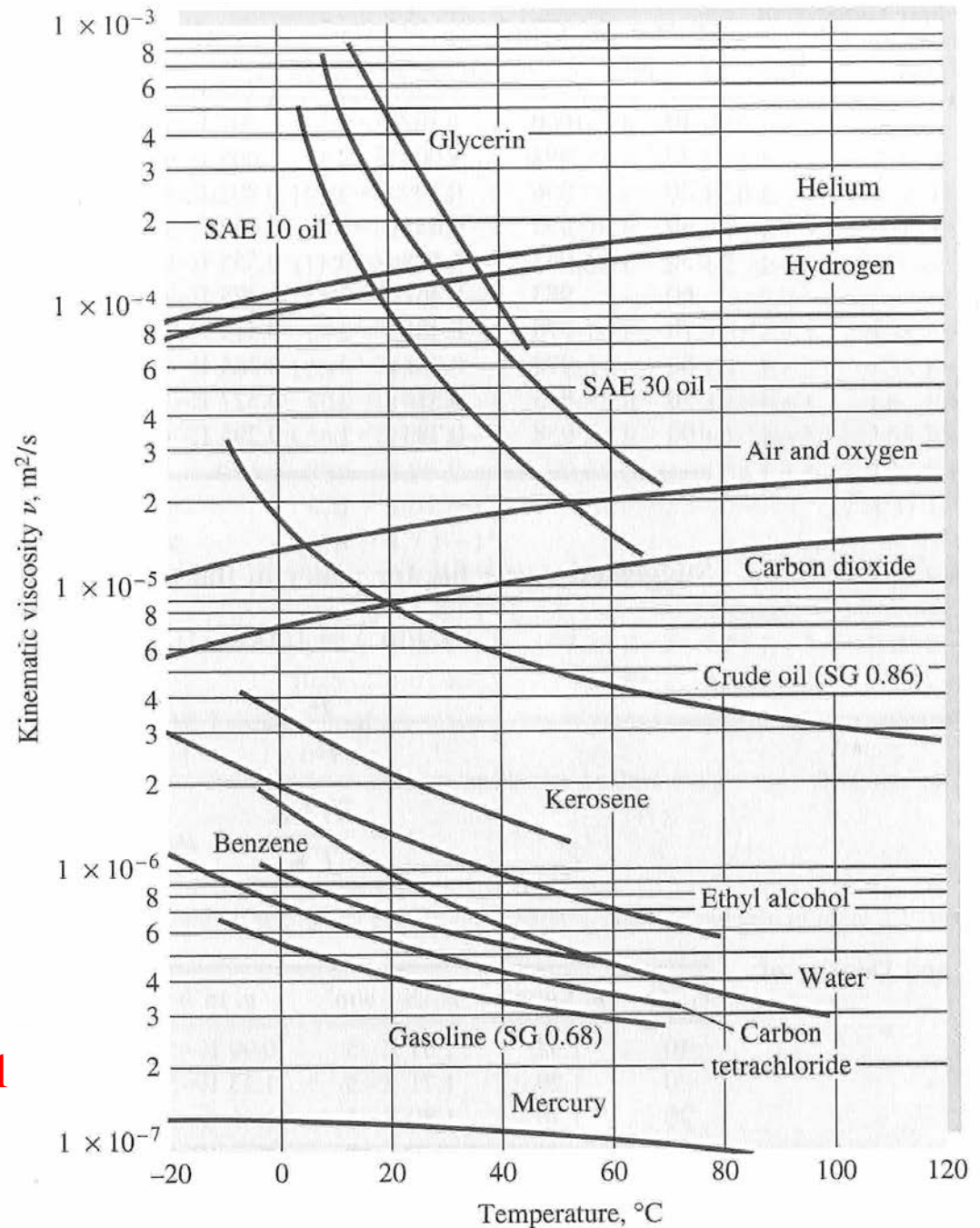
- Equal ratio between inertia and viscous forces:

$$\frac{\text{Inertia forces}}{\text{Viscous forces}} = \frac{F_i}{F_v} \propto \frac{\rho U^2 L^2}{\mu UL} = \frac{\rho UL}{\mu} = \frac{UL}{\nu} = Re$$

- $\nu$  is the kinematic viscosity,  $\nu = \frac{\mu}{\rho}$  [m<sup>2</sup>/s]
- Equality in  $Re$  will ensure that viscous forces are correctly scaled

# Kinematic viscosity of fluids

(from White: Fluid Mechanics)



To obtain equality of both  $Fn$  and  $Rn$  for a ship model in scale 1:10:  $\nu_m = 3.5 \times 10^{-8}$



# Mach number $M_n$

- Equal ratio between inertia and elastic fluid forces:

$$\frac{F_i}{F_e} \propto \frac{\rho U^2 L^2}{\varepsilon_v E_v L^2}$$

- By requiring  $\varepsilon_v$  to be equal in model and full scale:

$$\left( \frac{\rho U^2 L^2}{\varepsilon_v E_v L^2} \right)_M = \left( \frac{\rho U^2 L^2}{\varepsilon_v E_v L^2} \right)_F$$

$$\frac{U_M}{\sqrt{E_{v,M}/\rho}} = \frac{U_F}{\sqrt{E_{v,F}/\rho}} = M_n$$

- $\sqrt{E_v/\rho}$  is the speed of sound
- Fluid elasticity is very small in water, so usually Mach number similarity is not required
  - It is only when Mach numbers get close to 1 that it is important to consider compressibility effects. When  $Mach < 0.7$ , incompressible flow is assumed

# Weber number $W_n$

- The ratio between inertia and surface tension forces:

$$\frac{\text{Inertia forces}}{\text{Surface tension forces}} = \frac{F_i}{F_s} \propto \frac{\rho U^2 L^2}{\sigma L} = \frac{\rho U^2 L}{\sigma}$$

- Similarity requirement for model and full scale forces:

$$\left( \frac{\rho U^2 L}{\sigma} \right)_M = \left( \frac{\rho U^2 L}{\sigma} \right)_F$$

$$\sigma = 0.073 \text{ at } 20^\circ\text{C}$$

$$\frac{U_M}{\sqrt{\sigma_M / (\rho L)_M}} = \frac{U_F}{\sqrt{\sigma_F / (\rho L)_F}} = W_n$$

When  $W_n > 180$ , we assume that a further increase in  $W_n$  doesn't influence the fluid forces

# Scaling ratios used in testing of ships and offshore structures

Symbol	Dimensionless Number	Force Ratio	Definition
$R_e$	Reynolds Number	Inertia/Viscous	$\frac{UL}{\nu}$
$F_n$	Froude Number	Inertia/Gravity	$\frac{U}{\sqrt{gL}}$
$M_n$	Mach's Number	Inertia/Elasticity	$\frac{U}{\sqrt{E_v/\rho}}$
$W_n$	Weber's Number	Inertia/Surface tension	$\frac{U}{\sqrt{\sigma/\rho L}}$
$St$	Strouhall number	-	$\frac{f_v D}{U}$
$KC$	Keulegan-Carpenter Number	Drag/Inertia	$\frac{U_A T}{D}$

# Froude Scaling

$$\frac{U_M}{\sqrt{gL_M}} = \frac{U_F}{\sqrt{gL_F}} \Rightarrow U_F = U_M \sqrt{\frac{L_F}{L_M}} = U_M \sqrt{\lambda}$$

Using the geometrical similarity requirement:  $\lambda = L_F / L_M$

If you remember this, most of the other scaling relations can be easily derived just from the physical units

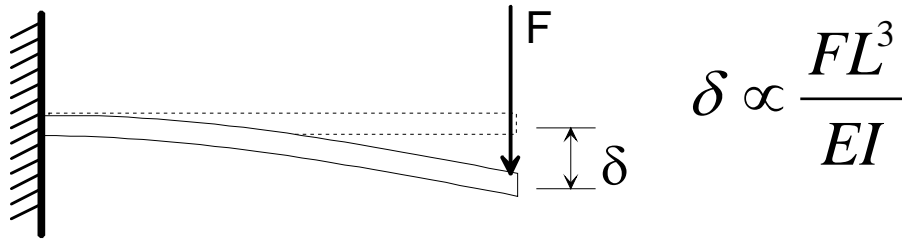
# Froude scaling table

Physical Parameter	Unit	Multiplication factor
Length	[m]	$\lambda$
Structural mass:	[kg]	$\lambda^3 \cdot \rho_F / \rho_M$
Force:	[N]	$\lambda^3 \cdot \rho_F / \rho_M$
Moment:	[Nm]	$\lambda^4 \cdot \rho_F / \rho_M$
Acceleration:	[m/s <sup>2</sup> ]	$a_F = a_M$
Time:	[s]	$\sqrt{\lambda}$
Pressure:	[Pa=N/m <sup>2</sup> ]	$\lambda \cdot \rho_F / \rho_M$

# Hydroelasticity

- Additional requirements to the elastic model
  - Correctly scaled global stiffness
  - Structural damping must be similar to full scale
  - The mass distribution must be similar
- Typical applications:
  - Springing and whipping of ships
  - Dynamic behaviour of marine risers and mooring lines

# Scaling of elasticity



Hydrodynamic force:

$$F \propto C\rho U^2 L^2$$

Geometric similarity requirement:

$$\frac{\delta_F}{L_F} = \frac{\delta_M}{L_M} \Rightarrow \delta_F = \lambda \delta_M$$

Requirement to structural rigidity:

$$\left( \frac{U^2 L^4}{EI} \right)_F = \left( \frac{U^2 L^4}{EI} \right)_M \Rightarrow (EI)_F = (EI)_M \lambda^5$$

# Scaling of elasticity

## – geometrically similar models

- Geometrically similar model implies:  $I_F = I_M \lambda^4$
- Must change the elasticity of material:  $E_F = E_M \lambda$
- Elastic propellers must be made geometrically similar, using a very soft material:  $E_M = E_F / \lambda$
- Elastic hull models are made geometrically similar only on the outside. Thus, E is not scaled and  $I_M = I_F \cdot \lambda^{-5}$



# Cavitation

- Dynamic similarity requires that cavitation is modelled
- Cavitation is correctly modelled by equality in cavitation number:

$$\sigma = \frac{(\rho gh + p_0) - p_v}{1/2 \rho U^2}$$

- To obtain equality in cavitation number, atmospheric pressure  $p_0$  might be scaled
- $p_v$  is vapour pressure and  $\rho gh$  is hydrostatic pressure
- Different "definitions" of the velocity  $U$  is used

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